

## Suggested Solutions for Mid-term Exam.

1 a)  $I_{D1} = I_{D2} = I_{D6} = I_B/2$

$I_{D8} = NI_B/2$

$\Delta V_n = \sqrt{I_B / K_n' \frac{W}{L}}$

 $n = 1, 2, 3, 4, 6, 7, 8$ 

$\Delta V_9 = \sqrt{I_B / \frac{K_n' W}{2L}}$

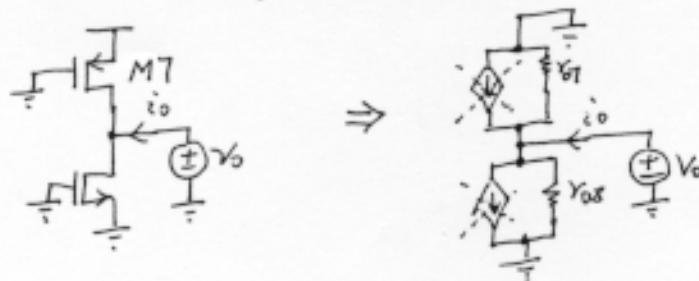
$\Delta V_P = \sqrt{I_B / K_p' \frac{W}{L}}$

 $P = 3, 4, 5, 7$ 

b)  $V_{SS} + \Delta V_9 + V_{T_{1,2}} + \Delta V_{1,2} < V_{1cm} < V_{DD} - |V_{T_{3,4}}| - |\Delta V_{3,4}| + V_{T_{4,2}}$

c)  $V_{SS} + \Delta V_8 \leq V_o \leq V_{DD} - |\Delta V_7|$

d)  $\therefore R_{out} = \frac{V_o}{i_o} \Big|_{V_{in}=0}$

 $\therefore$  The small signal model becomes.

$\therefore R_{out} = Y_{O7} // Y_{O8} \cancel{\times}$

e). For a common source amplifier,

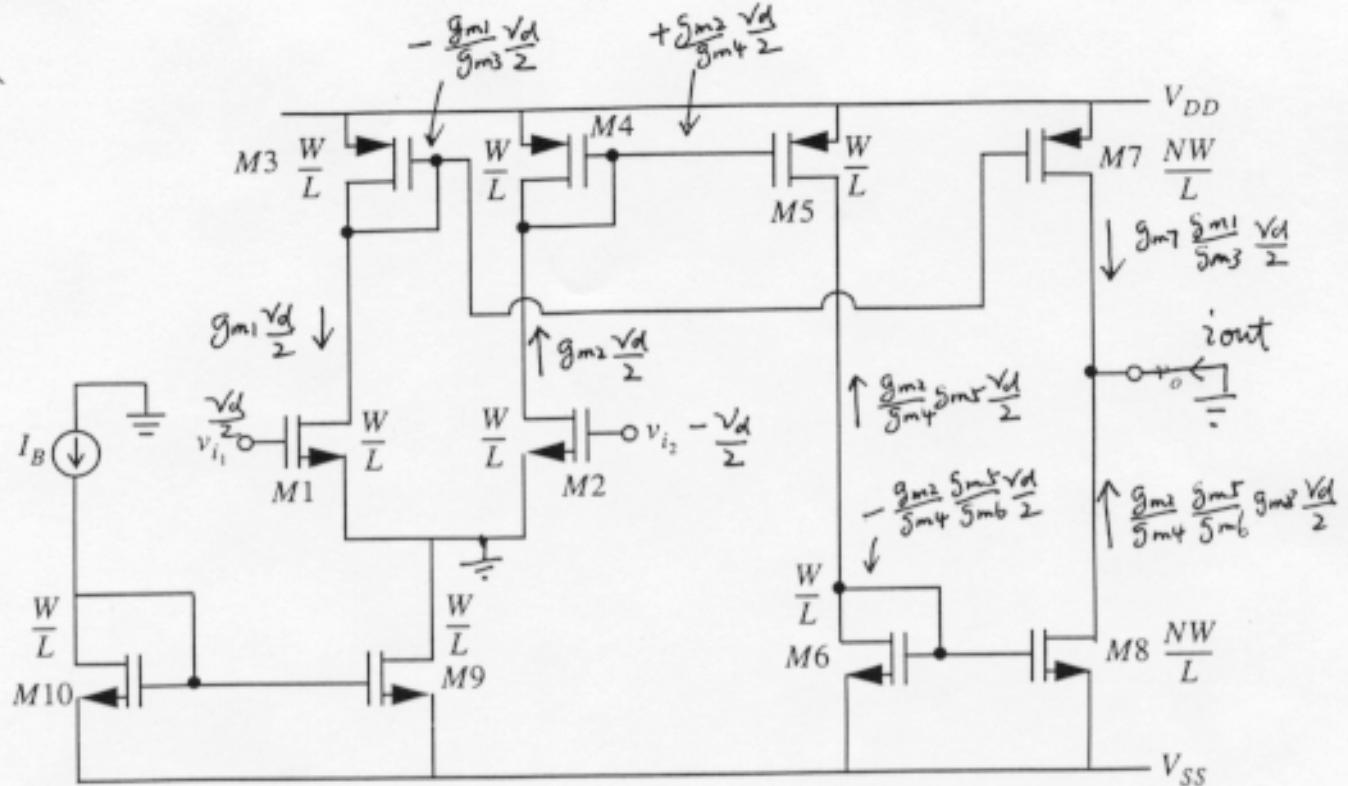
$$v_i \rightarrow \boxed{i_{ds}} \Rightarrow v_i \rightarrow \boxed{g_m v_i \approx Y_O} \Rightarrow i_{ds} = g_m v_i \text{ if } Y_O \gg \frac{1}{g_m}$$

For differential mode input,  $v_{i1} = \frac{v_d}{2}$ ,  $v_{i2} = -\frac{v_d}{2}$ ,

and the drain of M9 is a.c. grounded (i.e. d.c. voltage is constant).

We can find  $G_m = \frac{i_{out}}{v_d} \Big|_{v_o=0}$  by using " $i_{ds} = g_m v_i$ "and working from  $M1 \rightarrow M3 \rightarrow M7$ +  $M2 \rightarrow M4 \rightarrow M5 \rightarrow M6 \rightarrow M8$  as indicated in the

figure:



$$\text{Therefore } i_{\text{out}} = - \left[ g_m \frac{g_m}{g_m} \frac{V_d}{2} + \frac{g_m}{g_m} \frac{g_m}{g_m} \frac{g_m}{g_m} \frac{V_d}{2} \right]$$

$$\therefore g_{m1} = g_{m2} = g_{m1,2}, Ng_{m3} = g_{m7}, g_{m4} = g_{m5}, g_{m6} \wedge v = g_{m8}$$

$$\therefore G_m = -Ng_{m1,2} \cancel{\times}$$

f) For common mode input, the circuit is symmetrical.

$$M_1 \rightarrow M_3 \rightarrow M_7 \rightarrow M_8 \quad vs \quad M_2 \rightarrow M_4 \rightarrow M_5 \rightarrow M_6$$

So,  $V_{D8} = V_{D6} = V_{G16} = V_{G8}$ ,  $\Rightarrow M8$  is diode connected in CM.

Use half circuit technique, we have

Since M9 is shared by the 2 half circuits,

$$\therefore R_s = 2r_{0g}$$

M1 then becomes a CS amplifier with degeneration,

$$\therefore i_{SD7} \approx i_{DS1N} = \frac{g_{m1}}{1 + g_{m1}^2 R_O} V_{DS1N}$$

$$\therefore V_0 = 1258 \left( \frac{1}{g_{mg}} \right)$$

$$= 2 \pi d_7 \left( \frac{1}{g_{m8}} \right) = \frac{g_{m1} N}{g_{m8}(1 + 2g_{m1} Y_{09})} V_{icm}$$

$$= \frac{Y_0}{V_{1cm}} = -\frac{1}{(1+2g_m Y_0 q)} \quad \cancel{\#}$$

$$2 \text{ a) } I_{\text{out}} = I_{\text{ref}}$$

$$V_{GSn} = \sqrt{\frac{2I_{\text{ref}}}{k'(\frac{W}{L})}} + V_{Tn}, \quad n = 1, 2, 4, 5$$

$$V_{Gn} = \sqrt{\frac{2I_B}{k'(\frac{W}{L})}} + V_{Tn}, \quad n = 3, 6$$

$$\text{b) } V_{\text{out min}} = \Delta V_2 + V_{GS3} = \Delta V_2 + V_{T3} + \Delta V_1$$

$$= \sqrt{\frac{2I_{\text{ref}}}{k'(\frac{W}{L})}} + \sqrt{\frac{2I_B}{k'(\frac{W}{L})}} + V_{T3}$$

c) Ignore body effect

$$\therefore \frac{V_2}{Y_{O3}} = -g_{m3} V_1$$

$$\therefore V_2 = -g_{m3} Y_{O3} V_1 \quad (1)$$

$$\text{Also, } \frac{V_1}{Y_{O1}} = i_t \quad (2)$$

$$\frac{V_t - V_1}{Y_{O2}} + g_{m2}(V_2 - V_t) = i_t \quad (3)$$

$$\text{Sub (1) + (2) into (3)} \quad \frac{V_t}{Y_{O2}} + g_{m2}(-g_{m3} Y_{O3} Y_{O1} i_t) - g_{m2} Y_{O1} i_t - \frac{Y_{O1} i_t}{Y_{O2}} = i_t$$

$$\therefore R_{\text{out}} = \frac{V_t}{i_t} = Y_{O1} + Y_{O2} + g_{m2} Y_{O1} Y_{O2} + g_{m2} g_{m3} Y_{O1} Y_{O2} Y_{O3}$$

$$\approx Y_{O1} Y_{O2} Y_{O3} g_{m2} g_{m3}$$



d) Ensure  $V_{O4} = V_{O1}$  so that  $I_{\text{out}} = I_{\text{ref}}$  even there is channel length modulation.

